# Evaluation Board User Guide <br> UG-204 

## Evaluation Board for the ADP1850SP Step-Down DC-to-DC Controller

## FEATURES

Input range: 10 V to 20 V
Two output voltages: 3.3 V and 1.8 V
Output current: 14 A per channel
Switching frequency: 600 kHz
Operates in PWM or PSM
Compact, low cost, and efficient design

## EVALUATION BOARD DESCRIPTION

This document describes the design, operation, and test results of the ADP1850SP-EVALZ. The input range for this evaluation board is 10 V to 20 V , and the two regulated output voltages are set to 3.3 V (Vout1) and 1.8 V (Vout2) with a maximum 14 A output current. A switching frequency ( $\mathrm{fsw}_{\mathrm{sw}}$ ) of 600 kHz is chosen to achieve a good balance between efficiency and the sizes of the power components.

## ADP 1850 DEVICE DESCRIPTION

The ADP1850 is a dual-channel, step-down switching controller with integrated drivers for external N -channel synchronous
power MOSFETs. The two PWM outputs are phase shifted $180^{\circ}$, which reduces the input RMS ripple current, thus minimizing required input capacitance. The two outputs can be combined for dual-phase PWM operation that can deliver more than 50 A output current. The internal parameters of the two channels are optimized for current sharing.
In addition, boost diodes are integrated into the ADP1850, thus lowering the overall system cost and component count. The ADP1850 can be set to operate in pulse skip, high efficiency mode under light load or in PWM continuous conduction mode.
The ADP1850 includes externally adjustable soft start, output overvoltage protection, externally adjustable current limit, power good, tracking function, and a programmable oscillator frequency that ranges from 200 kHz to 1.5 MHz . The ADP1850 provides an output voltage accuracy of $\pm 0.85 \%$ from $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ and $\pm 1.5 \%$ from $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ junction temperature. This controller can be powered from a 2.75 V to 20 V supply and is available in a 32 -lead $5 \mathrm{~mm} \times 5 \mathrm{~mm}$ LFCSP package.


Figure 1.

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## REVISION HISTORY

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## COMPONENT DESIGN

For information about selecting power components and calculating component values, see the ADP1850 data sheet.

## INDUCTOR SELECTION

A $1.2 \mu \mathrm{H}$ inductor with a 20 A average current rating (744325120 from Würth Elektronik) is selected. This is a compact inductor with a ferrite core, which offers high performance in terms of low $\mathrm{R}_{\mathrm{DC}}$ and low core loss.

## INPUT CAPACITORS

Because of the very low ESR and high input current rating of multilayer ceramic capacitors (MLCCs), two $10 \mu \mathrm{~F}$ MLCCs in Size 1210 are selected as the input capacitors at the input of each channel. In addition, a $150 \mu \mathrm{~F}$ bulk OS-CON ${ }^{\text {mp }}$ (aluminum solid capacitor with conductive polymer) capacitor from Sanyo is chosen for filtering out any unwanted low-frequency noise from the input power supply.

## OUTPUT CAPACITORS

A combination of POSCAP ${ }^{m \times 1}$ polymer capacitors and MLCCs are selected for the output rails. Polymer capacitors have low ESR and high current ripple rating. Connecting polymer capacitors and MLCCs in parallel is very effective in reducing voltage ripple. Two $330 \mu \mathrm{~F}$ POSCAP capacitors and two $22 \mu \mathrm{~F}$ MLCCs are selected for each output.

## MOSFET SELECTION

For low output or low duty cycle, select a high-side MOSFET with fast rise and fall times and with low input capacitance to minimize charging and switching power loss. As for the synchronous rectifier (low-side MOSFET), select a MOSFET with low $R_{D s o N}$ because the switching speed is not critical and there is no switching power loss in the low-side MOSFET.

For the high-side MOSFET, the BSC080N03LS from Infineon Technologies in the PG-TDSON-8 or Super-SO8 package is selected. This part has low input capacitance ( 1.2 nF ) and fast transition times ( 3 ns ). For the low-side MOSFET, the BSC030N03LS, with RDSon of $4.7 \mathrm{~m} \Omega$ at a $\mathrm{V}_{\mathrm{GS}}$ of 4.5 V , is selected.

## TEST RESULTS

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.


Figure 2. Efficiency (Measurement Is Made with the Adjacent Channel Disabled)


Figure 3. Line Regulation


Figure 4. Load Regulation


Figure 5. Output Ripple, 14 A Load


Figure 6. Step Load Transient, Vout1


Figure 7. Step Load Transient, Vout2

## EVALUATION BOARD OPERATING INSTRUCTION

1. Connect Jumper J3 (EN1) to the high position to enable Channel 1 of the ADP1850.
2. Connect Jumper J2 (EN2) to the high position to enable Channel 2 of the ADP1850.
3. Connect Jumper J4 (FREQ) to the high position for 600 kHz operation.
4. Connect Jumper J1 (SYNC) to the high position for PWM operation or to low for PSM operation.
5. Connect the positive terminal of the input power supply to the input terminal, T1. The input range is 10 V to 20 V .

Table 1. Jumper Description

| Jumper | Description | Default Factory <br> Setting | Function |
| :--- | :--- | :--- | :--- |
| J1 | SYNC | High | Connect high for PWM or low for PSM operation. For synchronization, run an external clock <br> source to this pin. |
| J2 | EN2 | High | Connect high to enable Channel 2 of the ADP1850 or low to disable the channel. <br> Connect high to enable Channel 1 of the ADP1850 or low to disable the channel. <br> J3 |
| EN1 | FREQ | High |  |
| High | operation at 600 kHz . Connect J4 high. |  |  |

Table 2. Performance Summary ( $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ )

| Parameter | Condition |
| :---: | :---: |
| $\mathrm{V}_{\mathrm{IN}}$ | 10 V to 20 V |
| fsw | Switching frequency, 600 kHz |
| Vout1 | 3.3 V |
| lout1 | 0 A to 14 A |
| Vout1 Ripple, DC Load | 18 mV at 14 A load |
| Vout1 Deviation upon Step Load Release | $1.5 \%$ with a 7 A step load |
| $V_{\text {OUT2 }}$ | 1.8 V |
| lout2 | 0 A to 14 A |
| Vout2 Ripple, DC Load | 18 mV at 14 A load |
| $V_{\text {out2 }}$ Deviation upon Step Load Release | $1.8 \%$ with a 7 A step load |

## OTHER INFORMATION ABOUT THE EVALUATION BOARD PCB LAYOUT

As seen in Figure 1, the layout of this evaluation board is not optimized for the smallest PCB area. It is laid out in such a way that any of the components can be desoldered and replaced easily with different components with a hand soldering iron so that the user can modify the existing design without acquiring a new PCB layout. The physical size of the compensation components is 0603, which is selected for its ease of hand soldering when reworking the board is needed. The size of these components can be 0402 or even smaller in the final design. Note that there are extra place holders for input bulk capacitors, output filter capacitors, and MOSFETs. The user can remove, add, or change any of these power components to achieve a particular design objective. The track functions,
where TRK1 and TRK2 are pulled up to VCCO through $0 \Omega$ dummy resistors, are not used on this evaluation board. If a tracking function is needed, the user can remove the $0 \Omega$ dummy resistors and add external resistive components to obtain the desired tracking function. Dummy $0 \Omega$ resistors are placed at the driver gates, DHx and DLx, for evaluation purpose only and can be removed in the final design. Also, the configuration of this evaluation board can be modified to obtain a single output dual-phase operation. Furthermore, many test points are placed on the evaluation board so that the user can easily evaluate the performances of the ADP1850 with an oscilloscope. See Figure 8, the evaluation board schematic, for more information.

## EVALUATION BOARD SCHEMATICS AND ARTWORK



Figure 8. Evaluation Board Schematic


Figure 9. Top Silkscreen


Figure 10. Top Layer


Figure 11. Second Layer (AGND Plane)


Figure 12. Third Layer (PGND Layer)


Figure 13. Bottom Layer (PGND Layer)


Figure 14. Bottom Silk Screen

## Evaluation Board User Guide

## ORDERING INFORMATION

## BILL OF MATERIALS

Table 3.

| Qty | Reference Designator | Description | Manufacturer | Part No. |
| :---: | :---: | :---: | :---: | :---: |
| 1 | U1 | Device under test, LFCSP | Analog Devices | ADP1850 |
| 1 | CIN20 | OS-CON, $150 \mu \mathrm{~F}, 20 \mathrm{~V}$ | Sanyo | 20SEP150M |
| 4 | CIN11, CIN12, CIN21, CIN22 | Input capacitor MLCC, $10 \mu \mathrm{~F}, \mathrm{X} 7 \mathrm{R}, 25 \mathrm{~V}$, 1210 | Murata | GRM32DR71E106KA12 |
| 5 | CSS1, CSS2, CBST1, CBST2, CVIN | Input capacitor MLCC, 100 nF, X7R, 25 V, 0603 | Murata | GRM188R71E104KA01 |
| 2 | CV5, CDR | Input capacitor MLCC, $1.0 \mu \mathrm{~F}, \mathrm{X} 5 \mathrm{R}$, $6.3 \mathrm{~V}, 0603$ | Murata | GRM185R60J105KE21 |
| 2 | RBO, RVCCO | Resistor, $2 \Omega, 0603$ | Vishay | CRCW06032R00F |
| 2 | RGCS1, RGCS2 | Resistor, $22.6 \mathrm{k} \Omega, 0603$ | Vishay | CRCW06032262F |
| 2 | RR1, RR2 | Resistor, $187 \mathrm{k} \Omega, 0603$ | Vishay | CRCW06031873F |
| 4 | COV1 COV11, COV2, COV21 | POSCAP, $330 \mu \mathrm{~F}, 6.3 \mathrm{~V}, 18 \mathrm{~m} \Omega$ | Sanyo | 6TPE330MFL |
| 4 | COV12, COV13, COV22, COV23 | MLCC, $22 \mu \mathrm{~F}, \mathrm{X} 5 \mathrm{R}, 1206$ | Murata | GRM31CR60J226ME19L |
| 2 | L1, L2 | Inductor, $1.2 \mu \mathrm{H}, 1.8 \mathrm{~m} \Omega, \mathrm{I}_{\mathrm{N}}=20 \mathrm{~A}$, $\mathrm{I}_{\text {SAT }}=25 \mathrm{~A}$ | Würth Elektronik | 744325120 |
| 2 | RF22, RF12 | Resistor, $10 \mathrm{k} \Omega, 0603$ | Vishay | CRCW06031002F |
| 1 | RF21 | Resistor, $20 \mathrm{k} \Omega, 0603$ | Vishay | CRCW06032002F |
| 1 | RF11 | Resistor, $45.3 \mathrm{k} \Omega, 0603$ | Vishay | CRCW06034532F |
| 8 | RDH1, RDH2, RDL1, RDL2, Rt11, Rt21, R1, R2 | Resistor, 0 , 0603 | Vishay | CRCW06030R00F |
| 2 | QH1, QH3 | N MOSFET, $30 \mathrm{~V}, 9 \mathrm{~m} \Omega$, super-SO8 | Infineon | BSC080N03LS |
| 2 | QL2, QL3 | N MOSFET, $30 \mathrm{~V}, 4.5 \mathrm{~m} \Omega$, super-SO8 | Infineon | BSC030N03LS |
| 1 | CC11 | MLCC, 330 pF , 0603 | Vishay | VJ0603Y331KXAA |
| 1 | CC21 | MLCC, 560 pF , 0603 | Vishay | VJ0603Y561KXAA |
| 2 | CC12, CC22 | MLCC, 47 pF, 0603 | Vishay | VJ0603A470KXAA |
| 1 | RC1 | Resistor, $42.2 \mathrm{k} \Omega, 0603$ | Vishay | CRCW06034222F |
| 1 | RC2 | Resistor, $23.2 \mathrm{k} \Omega, 0603$ | Vishay | CRCW06032322F |
| 2 | RLIM11, RLIM21 | Resistor, $2.1 \mathrm{k} \Omega, 0603$ | Vishay | CRCW06032101F |
| 2 | CLIM, CLIM2 | MLCC, 22 pF, 0603 |  | VJ0603A220KXAA |
| 4 | J1, J2, J3, J4 | 3-terminal jumpers, 0.1 inch Spacing | Any |  |
| 5 | T8, T9, T10, T11, T12 | Test points, 110 mil through hole | Keystone Electronics Corp. | 1502-1 |
| 6 | T1, T2, T3, T4, T5, T6 | Terminals | Keystone Electronics Corp. | 8191 |

ESD Caution
ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

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